

TABLE I

Type	Material	Specific Resistance (ohm-cm)	Holder	Commercial or Experimental
GSB1	Ge	0.05	1N263 Type	Commercial
GSB2	Ge	0.1	1N263 Type	Commercial
SiSBR	Si	0.03	1N263 Type	Experimental
SiSBR	Si	0.1-0.08	1N263 Type	Experimental

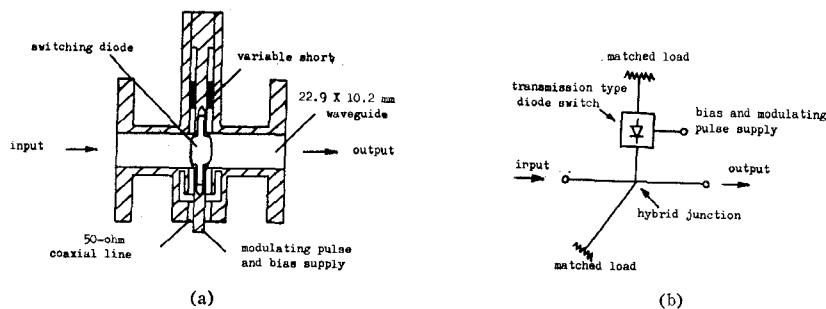


Fig. 1—Construction of diode switches.

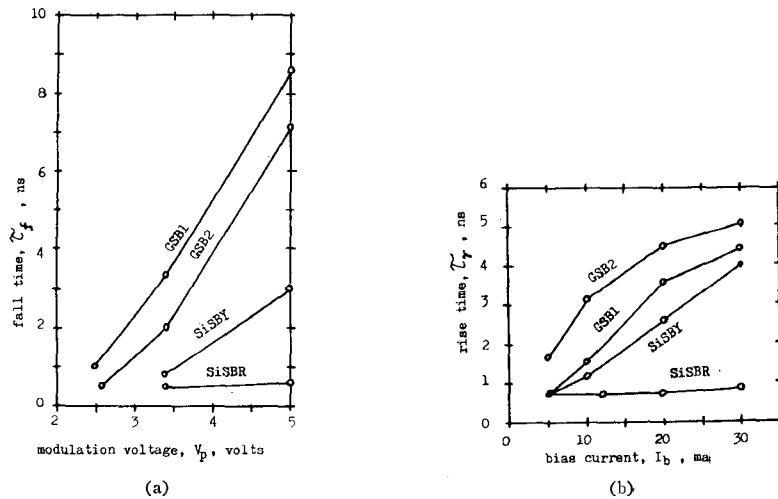
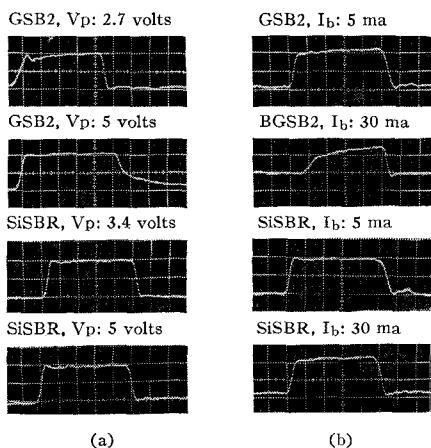


Fig. 2—Rise and fall times of diode switches in the conducting case. (a) Transmission type (microwave input power = 5 mw, static bias voltage = -5 v). (b) Reflection type (microwave input power = 5 mw, applied pulse voltage = 2 v).

Fig. 3—Microwave pulse waveforms (in-phase components) of diode switch output.  $V_p$  = applied pulse voltage,  $I_b$  = static bias current, horizontal axis = 2 nsec/div. (a) Transmission type (microwave input power = 5 mw, static bias voltage = -5 v). (b) Reflection type (microwave input power = 5 mw, applied pulse voltage = 2 v).

the hole storage effect. The switching fall time was almost independent of the static bias current and was about 0.5-0.7 nsec.

Fig. 3 illustrates the typical waveforms (in-phase components) of switched microwave pulses when the GSB2 and SiSB diodes are applied with a rectangular pulse of 20 nsec in the transmission and reflection-type switches.

It was concluded that the silicon silver-bonded diode SiSBR has the best rise and fall times: about 0.5 nsec.

#### ACKNOWLEDGMENT

The authors wish to thank Dr. B. Oguchi and Dr. S. Kita for their helpful discussions, and R. V. Garver for his encouragement.

KAZUHIRO MIYAUCHI  
OSAMU UEDA  
Electrical Communication Lab.  
Tokyo, Japan

#### Addendum to "An Exact Method for Synthesis of Microwave Band-Stop Filters"

##### SUMMARY

An algorithm is presented that enables a designer to compute efficiently and quickly the design parameters of microwave band-stop filters that are based on the exact synthesis technique previously discussed by Schiffman and Matthei. Tables of band-stop filter designs that give maximally flat and Chebyshev responses are presented for ten typical stop-band fractional bandwidths.

##### INTRODUCTION

By extending work of Ozaki and Ishii [1], Schiffman and Matthei [2], [3] have presented a theory and several design equations for an exact method of synthesizing microwave band-stop filters. Using their synthesis procedure, a band-stop filter is developed from a low-pass, lumped-element prototype filter. The band-stop filter is composed of either quarter-wavelength short-circuited stubs connected in series with the main transmission line, or quarter-wavelength open-circuited stubs connected in shunt with the main transmission line. The stubs are spaced at either quarter- or three-quarter-wavelengths. The characteristic admittances of the stubs and connecting lines depend on the low-pass filter that is used as a prototype. If the low-pass prototype filter has an attenuation function  $L_A(\omega'/\omega_1')$ , the band-stop filter will have a response  $L_A\{\Lambda \tan [(\pi/2)(\omega/\omega_0)]\}$  where  $L_A$  is the transducer attenuation in decibels. The arguments of the attenuation function  $L_A$  are defined as follows:

$\omega'$  is the frequency variable of the low-pass prototype filter,  
 $\omega_1'$  is the cutoff frequency of the low-pass prototype filter,  
 $\omega$  is the frequency variable of the band-stop filter,  
 $\omega_0$  is the center frequency of the band-stop filter,  
 $\Lambda$  is a scaling parameter that is defined

$$\Lambda = \omega_1' \tan [(\pi/4)w]. \quad (1)$$

The symbol  $w$  in (1) is the fractional stop bandwidth of the band-stop filter. It is defined by

$$w = \frac{\omega_2 - \omega_1}{\omega_0}, \quad (2)$$

where  $\omega_2$  and  $\omega_1$  are the cutoff frequencies of the band-stop filter corresponding to  $\omega_1'$  of the low-pass prototype filter.

Figs. 1(a) and 1(b) show configurations of the low-pass prototype filter used in the synthesis procedure. Note that the parameters  $g_i$  of the prototype filter are also defined in Figs. 1(a) and 1(b). Figs. 1(c) and 1(d) show typical maximally flat and Chebyshev responses of the filters of Figs. 1(a) and 1(b), respectively. Tables of  $g_i$

that give maximally flat or Chebyshev responses are presented in the literature [4], [5]. Figs. 2(a) and 2(b) show the derived band-stop filter using short-circuited and open-circuited stubs, respectively. The filters of Figs. 2(a) and 2(b) use quarter-wavelength connecting lines, while in Figs. 3(a) and 3(b), page 372, the filters are shown using three quarter-wavelength connecting lines. Note also that in Figs. 2(a), 2(b), 3(a) and 3(b), the parameters  $h_i$ ,  $h_{i+1}$  and  $(h_i, h_{i+1})$  are defined. These parameters are characteristic impedances or admittances of the transmission lines. They correspond to the  $g_i$  of the lumped-prototype filter. Fig. 4 shows an idealized response of the bandstop filter when designed from a Chebyshev prototype. The steady-state response would be the same for all the filters shown in Figs. 2 and 3.

In [2] and [3], equations are given for the cases of  $n=1$  through 5 resonators, that relate the  $g_i$  of the low-pass prototype filter to the  $h_i$  and  $h_{i+1}$  of the band-stop filter with quarter-wavelength spacing between stubs. Also, equations are presented for  $n=1, 2$  and 3, relating the  $g_i$  of the prototype filter to the  $h_i$  and  $(h_i, h_{i+1})$  of the band-stop filter with three-quarter wavelength spacing. Although it is desirable to have expressions for larger values of  $n$ , they have not been developed because the algebra is unwieldy. Also, (particularly for filters with three-quarter wavelength spacing between stubs), the formulas for large  $n$  would probably require longer computational time than the method that will be presented in this communication. For these reasons, an algorithm that systematically calculates the  $h$  parameters of the band-stop filter has been developed. The algorithm is a twofold iterative procedure that can be applied to a low-pass prototype filter of the type shown in Fig. 1 having any number of  $g$ 's. When the algorithm is used in conjunction with a desk calculator, most filter designs can be computed in 30 minutes or less, depending on the magnitude of  $n$ . (The first design example presented in this communication has  $n=8$ , and was computed in less than 25 minutes on a Friden desk calculator.)

#### AN ALGORITHM FOR THE $h$ PARAMETERS OF EXACT-DESIGNED BAND-STOP FILTERS

The algorithm is best explained by presenting two examples. The first example presents the computation of the  $h$  parameters of a band-stop filter that has eight stubs separated by quarter-wavelength lines. The filter has a 50 per cent stop-band bandwidth. It is based on an  $n=8$ , 0.5-db ripple, Chebyshev prototype filter. The  $g_i$  of the prototype filter are given in Table I [5].

To compute the  $h$ 's, the  $g_i$  are first modified by multiplying  $g_1$  through  $g_n$  (but not  $g_0$  or  $g_{n+1}$ ) by  $\Lambda$ , where recall that  $\Lambda=\omega_1 \tan[(\pi/4)w]$ . The modified  $g_i$  will be denoted as  $g'_i$ . They are given in Table II, page 373. Next, a computation matrix is begun in the manner shown in Fig. 5(a). Referring to Fig. 5(a), note that the number of  $(g'_i)$ 's to be placed in the zero column (the first column on the left) is given by the

value of the parameter  $P$ . The following rules are used to determine the value of  $P$ : if  $n$  is odd,

$$P = \frac{n}{2} - \frac{1}{2}; \quad (3)$$

if  $n$  is even,

$$P = \begin{cases} \frac{n}{2} - 1, & \text{in the development of the} \\ \frac{n}{2}, & \text{first half of the filter} \\ & \text{in the development of the} \\ & \text{second half of the filter.} \end{cases} \quad (4)$$

In the example being worked,  $n$  is 8. Therefore,  $P=(8/2)-1=3$  for the development of the first half of the filter. Next, we proceed to compute the entries in the matrix. To compute an entry in an odd-numbered column, use the rule shown in Fig. 5(b). For example, the entry in the square obtained from the intersection of the row and column marked 1 is given by  $[1/(0+1)]=1$ . The remaining entries in column 1 are computed in the same way and appear in Fig. 5(c).

To compute an entry in an even-numbered column, use the rule shown in Fig. 5(d). For example, the entry in the square obtained from the intersection of the row marked 1 and the column marked 2 is given by  $[(1 \times 0)/1]=0$ . The remaining entries in column 2 are computed in the same way and appear in Fig. 5(e). Next, using the appropriate rule for each column, the remaining entries of the matrix are computed. The result is given in Fig. 5(f).

The  $h$  parameters appear in the last row of the matrix as shown in Fig. 5(f). The terminating parameter corresponding to the source admittance is denoted by  $h_0$ . Its value appears in the last row and column. Adjacent to it is the first stub parameter,  $h_1$ . Adjacent to that is the connecting line parameter,  $h_{12}$ . Adjacent to that is a stub, etc.

If the band-stop filter is to be composed of short-circuited series stubs, the  $h$  parameters are in ohms. If the band-stop filter is to be composed of open-circuited shunt stubs, the  $h$  parameters are in mhos.

To calculate the  $h$  parameters of the second half of the band-stop filter, we use the preceding computational method but with  $g'$  values from the second half of the prototype filter. The computation matrix is begun as shown in Fig. 6(a), page 374. In this case,  $P=(8/2)=4$ , as given by (4). The entries in the matrix are computed using the same rules as before. The completed matrix is given in Fig. 6(b).

The reader may notice that the value of the parameter  $h_4$  has not been computed. It is given by the value of  $g'_4$ . In general, the value of the admittance of the "middle" stub is given by its  $g'$  counterpart. The following rules are a useful reminder.

$$\text{For } n \text{ even, } h_{n/2} = g'_{n/2}. \quad (5)$$

$$\text{For } n \text{ odd, } h_{n/2+1/2} = g'_{n/2+1/2}. \quad (6)$$

To calculate the  $h$  parameters of a band-stop filter with three-quarter wavelength spacing between stubs, use the previously explained algorithm but note the following

amendment. The initial setup of the computation matrix is modified as follows. In applying (3) or (4) to determine the parameter  $P$ , each  $g_i$  entry in the zero column of the computation matrix is followed by two zero entries. This procedure is demonstrated by the worked example given in Fig. 7(a) and 7(b), page 375.

The example given in Figs. 7(a) and 7(b) is for an  $n=4$ , 0.5-db ripple, Chebyshev band-stop filter having a 50 per cent stop-band bandwidth. The  $g_i$  and  $g'_i$  values are given in Tables III and IV, respectively [5]. Note in Figs. 7(a) and 7(b) that the effect of introducing zeros in the initial column of the matrix is to produce "dummy stubs" of zero characteristic admittance. These stubs are ignored in the synthesis of the filter. Note also that the indexing of the connecting lines is reversed in the computation matrix of the second half of the filter as compared to the indexing in the first half of the filter. This gives indexes for the final structure, which increase continuously from one end of the filter to the other.

As in the previous example,  $h_{n/2}$  is given by  $g'_{n/2}$  according to (5).

#### TABLES OF $h$ PARAMETERS FOR MAXIMALLY FLAT AND CHEBYSHEV BAND-STOP FILTERS

The algorithm previously given was programmed on an electronic digital computer and several tables of  $h$ 's (Tables V-IX, pages 376-382) compiled for maximally flat and Chebyshev band-stop filters having various fractional bandwidths  $w$ .

For  $n$  odd, only one half of the  $h$  parameters are presented in the tables because the filters are symmetrical about the center stub. In these cases, the  $h$  parameters obey the relationship

$$h_{n+1-i} = h_i \quad (7)$$

$$h_{n-i-n-i+1} = h_{i,i+1} \quad (8)$$

#### ACKNOWLEDGMENT

The computer programming of the algorithm for the tables of band-stop filter designs was done by P. H. Omlor. P. Rezek calculated the examples presented in the text.

E. G. CRISTAL  
Stanford Research Institute,  
Menlo Park, Calif.

#### REFERENCES

- [1] H. Ozaki and J. Ishii, "Synthesis of transmission-line networks and the design of UHF filters," *IRE TRANS. ON CIRCUIT THEORY*, vol. CT-2, pp. 325-336; December, 1955.
- [2] B. M. Schiffman, P. S. Carter, Jr. and G. L. Matthaei, "Microwave Filters and Coupling Structures," Stanford Research Institute, Menlo Park, Calif., Quarterly Progress Rept. No. 7, Contract DA 36-039 SC-87398, SRI Project 3527; October, 1962.
- [3] B. M. Schiffman and G. L. Matthaei, "An exact method for synthesis of microwave band-stop filters," *TRANS. IEEE ON MICROWAVE THEORY AND TECHNIQUES*, vol. MTT-12, pp. 6-15; January, 1964.
- [4] L. Weinberg, "Additional tables for design of optimum ladder networks," *J. Franklin Inst.*, pp. 7-23, July, 1957; pp. 127-138, August, 1957.
- [5] G. L. Matthaei, L. Young and E. M. T. Jones, "Design of Microwave Filters, Impedance-Matching Networks, and Coupling Structures," Stanford Research Institute, Menlo Park, Calif., vol. 1, pp. 98 and 100-102; Contract DA 36-039 SC-87398, SRI Project 3527, January, 1963.

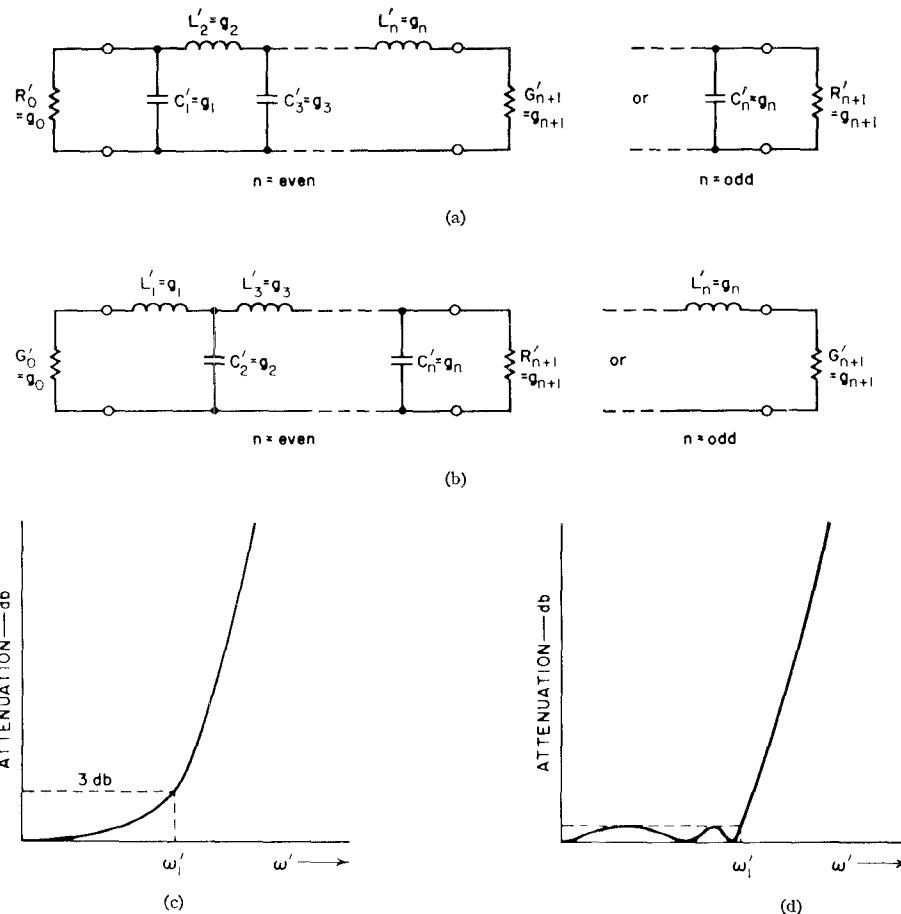


Fig. 1—Low-pass prototype filter: four basic circuit types defining the parameters  $g_0, g_1, \dots, g_{n+1}$  and maximally flat and equiripple characteristics defining the band edge  $\omega'_i$ .

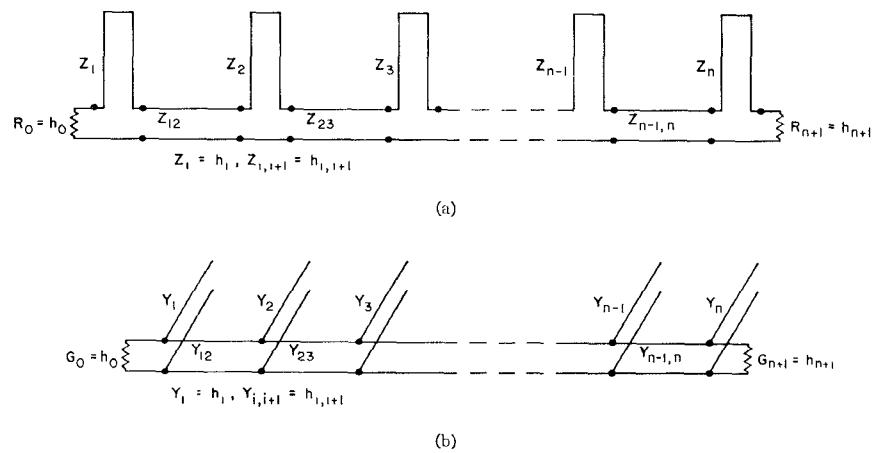


Fig. 2—Two dual band-stop filter structures using  $\lambda_0/4$  stubs and  $\lambda_0/4$  connecting lines, and definitions of  $h$  parameters. (a) Short-circuited stubs. (b) Open-circuited stubs.

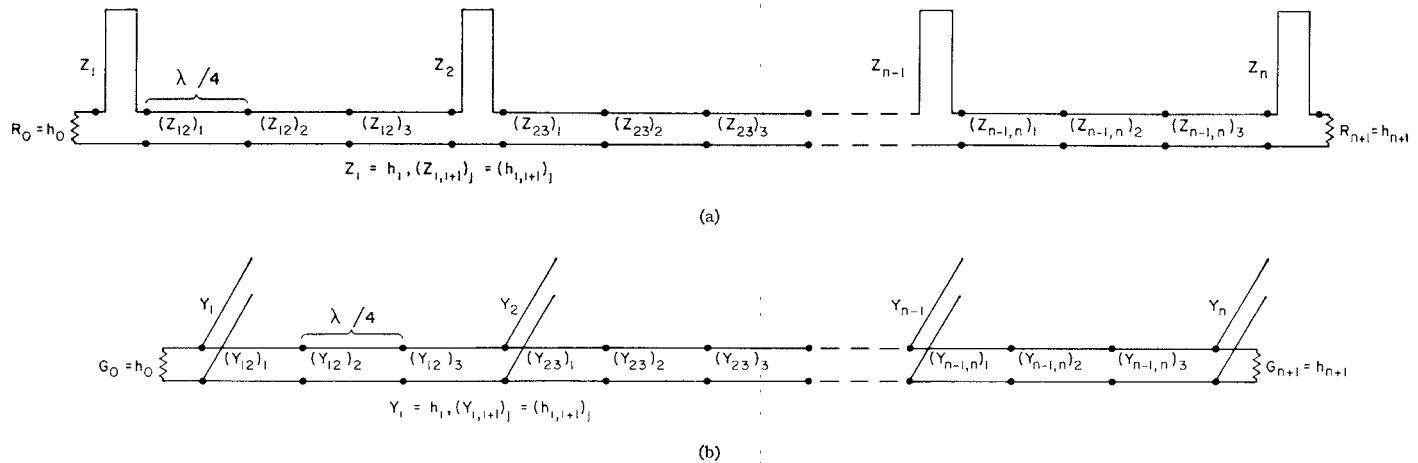


Fig. 3—Two dual band-stop filter structures using  $\lambda_0/4$  stubs and  $3\lambda_0/4$  connecting lines, and definitions of  $h$  parameters.  
 (a) Short-circuited stubs. (b) Open-circuited stubs.

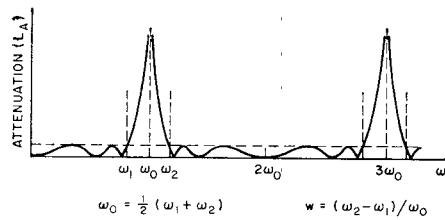


Fig. 4—Typical equiripple idealized response of band-stop filters designed on the exact basis.

TABLE I  
 $g$  VALUES FOR AN  $n = 8$ , 0.5-db CHEBYSHEV PROTOTYPE FILTER

$g_0$	$g_1$	$g_2$	$g_3$	$g_4$	$g_5$	$g_6$	$g_7$	$g_8$	$g_9$
1 0	1 7451	1 2647	2.6564	1.3590	2.6964	1.3389	2.5093	0.8796	1.9841

TABLE II  
 $g'$  VALUES USED IN THE FIRST EXAMPLE IN THE TEXT  
 $g_i' = \lambda g_i$   
 $\omega_1' = 1.0$

$g_0'$	$g_1'$	$g_2'$	$g_3'$	$g_4'$	$g_5'$	$g_6'$	$g_7'$	$g_8'$	$g_9'$
1.0	0.72284	0.52385	1.1003	0.56291	1.1169	0.55458	1.0394	0.36434	1.9841

P ELEMENTS  $g_i'$  AND P ROWS

2P + 1 COLUMNS							
0	1	2	3	4	5	6	7
0	$g_0' = 1.0$	0	$g_1' = 1.0$	0	$g_2' = 1.0$	0	$g_3' = 1.0$
1	$g_1' = 0.72284$						
2	$g_2' = 0.52385$						
3	$g_3' = 1.1003$						

(a)

0	1	2	3	4	5
0	XXXX	0	XXXX	0	XXXX
1	A	B			Given these entries.
2	XXXX	$\frac{1}{A+B}$			This entry is
3	XXXX				

(b)

0	1	2	3	4	5	6	7
0	1.0	0	1.0	0	1.0	0	1.0
1	0.72284	1.0					
2	0.52385	0.58044					
3	1.1003	0.90555					
		0.49855					

(c)

0	1	2	3	4	5	6	7
0	XXXX	0	XXXX	0	XXXX		
1	XXXX	XXXX	XXXX				
2	A	B	XXXX			Given these entries.	
3	XXXX	C	$\frac{(C \times A)}{B}$			This entry is	
		XXXX					

(d)

0	1	2	3	4	5	6	7
0	1	0	1	0	1	0	1
1	0.72284	1	0				
2	0.52385	0.58044	0.41956				
3	1.1003	0.90555	0.81726				
		0.49855	0.60576				

(e)

0	1	2	3	4	5	6	7
0	1	0	1	0	1	0	1
1	0.72284	1	0	1	0	1	0
2	0.52385	0.58044	0.41956	1	0	1	0
3	1.1003	0.90555	0.81726	0.70441	0.29555	1	0
		0.49855	0.60576	0.65716	0.76211	0.77187	0.22813
		$h_{34}$	$h_3$	$h_{23}$	$h_2$	$h_{12}$	$h_1$
							$h_0$

(f)

Fig. 5.—Example calculation of the  $h$  parameters of a band-stop 0.5-db ripple Chebyshev filter having eight stubs with quarter-wavelength spacing between stubs (first half of filter). (a) Start of computation matrix. (b) Rule for computing entries in odd-numbered columns. (c) Example calculation of column 1. (d) Rule for computing entries in even-numbered columns. (e) Example calculation of column 2. (f) Completed computation matrix.

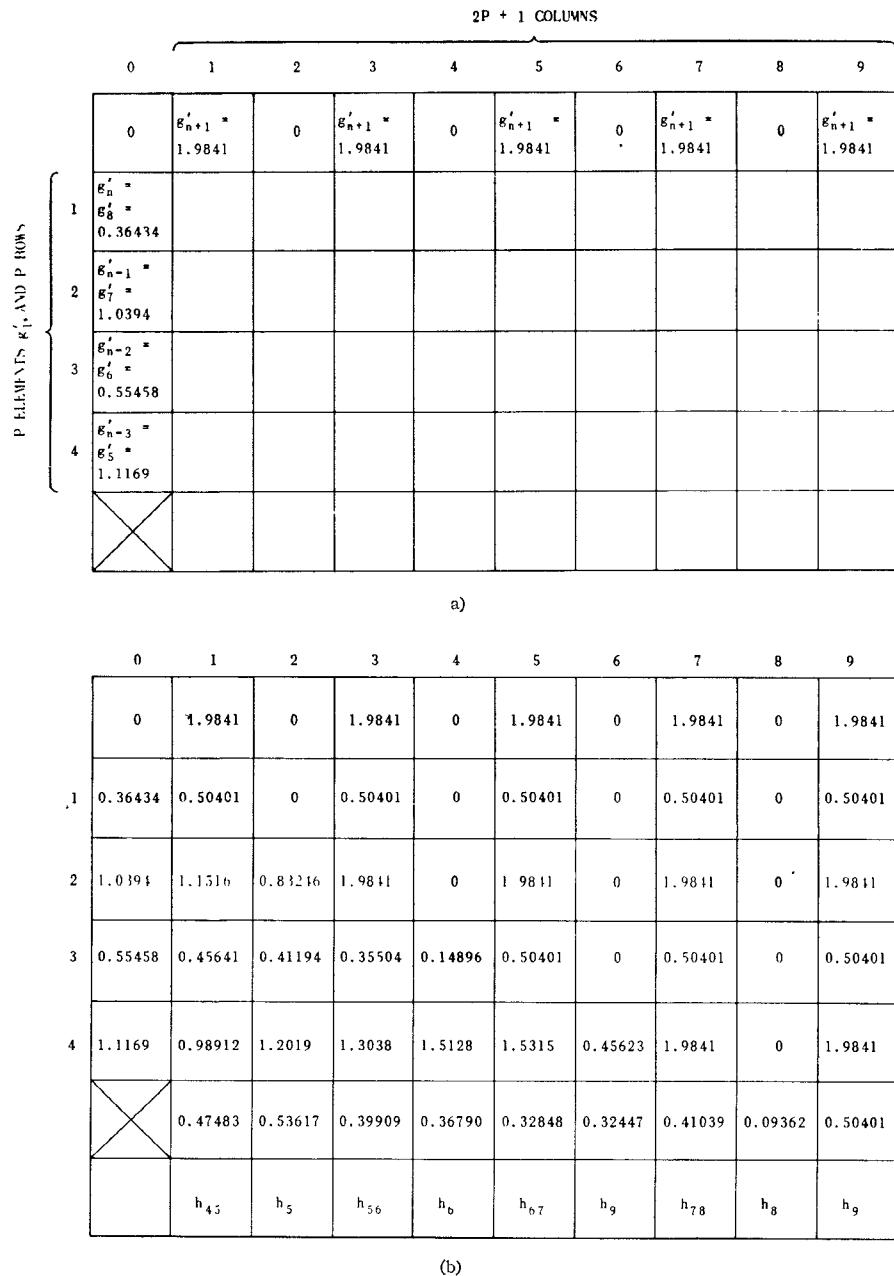


Fig. 6—Example calculation of the  $h$  parameters of a band-stop 0.5-db ripple Chebyshev filter having eight stubs with quarter-wavelength spacing between stubs (second half of filter).

2(3P) + 1 COLUMNS													
P ELEMENTS $g_1'$ AND 3P ROWS													
	0	1	0	1	0	1	0	1	0	1	0	1	
1	0.69185	1	0	1	0	1	0	1	0	1	0	1	
2	0	0.59107	0.40893	1	0	1	0	1	0	1	0	1	
3	0	1.69185	0	0.70976	0.29024	1	0	1	0	1	0	1	
	$(h_{12})_3$	DUMMY STUB	$(h_{12})_2$	DUMMY STUB	$(h_{12})_1$	$h_1$	$h_0$						
(a)													
2(3P) + 1 COLUMNS													
P ELEMENTS $g_1'$ AND 3P ROWS													
	0	1.9841	0	1.9841	0	1.9841	0	1.9841	0	1.9841	0	1.9841	
1	0.34872	0.50401	0	0.50401	0	0.50401	0	0.50401	0	0.50401	0	0.50401	
2	0	1.1727	0.81138	1.9841	0	1.9841	0	1.9841	0	1.9841	0	1.9841	
3	0	0.85273	0	0.35772	0.14629	0.50401	0	0.50401	0	0.50401	0	0.50401	
4	0.98006	1.1727	0	2.7956	0	1.5378	0.44634	1.9841	0	1.9841	0	1.9841	
5	0	0.4652	0.38821	0.35772	0	0.6503	0	0.41145	0.09256	0.50401	0	0.50401	
6	0	2.1527	0	1.3406	1.45486	1.5378	0	2.4304	0	1.67626	0.30782	1.9841	
	$(h_{23})_3$	DUMMY STUB	$(h_{23})_2$	DUMMY STUB	$(h_{23})_1$	$h_3$	$(h_{34})_1$	DUMMY STUB	$(h_{34})_2$	DUMMY STUB	$(h_{34})_3$	$h_4$	$h_5$
(b)													

Fig. 7.—(a) Example calculation of the  $h$  parameters of a band-stop 0.5-db ripple Chebyshev filter having four stubs with three-quarter wavelength spacing between stubs (first half of filter). (b) Example calculation of the  $h$  parameters of a band-stop 0.5-db ripple Chebyshev filter having four stubs with three-quarter wavelength spacing between stubs (second half of filter).

TABLE III  
 $g$  VALUES FOR AN  $n = 4$ , 0.5-db CHEBYSHEV  
PROTOTYPE FILTER

$g_0$	$g_1$	$g_2$	$g_3$	$g_4$	$g_5$
1.0	1.6703	1.1926	2.3661	0.8419	1.9841

TABLE IV  
 $g'$  VALUES USED IN THE SECOND EXAMPLE  
IN THE TEXT

$g_0'$	$g_1'$	$g_2'$	$g_3'$	$g_4'$	$g_5'$
1.0	0.69185	0.49399	0.98006	0.34872	1.9841

TABLE V  
 $h$  VALUES FOR MAXIMALLY FLAT FILTERS HAVING  $h_0$  AND  $h_{n+1} = 1.0$  AND VARIOUS STOP-BAND 3-DB FRACTIONAL BANDWIDTHS  $w$

$n = 2$										
$w$	0.02	0.05	0.10	0.20	0.30	0.50	0.70	1.00	1.40	1.80
$h_1$	.02221	.05556	.11128	.22396	.33947	.58570	.86650	1.4140	2.7751	8.9276
$h_{12}$	.97827	.94737	.89986	.81702	.74656	.63064	.53576	.41425	.26489	.10073
$h_2$	.02173	.05263	.10014	.18298	.25344	.36936	.46424	.58575	.73511	.89927

$n = 3$										
$w$	0.02	0.05	0.10	0.20	0.30	0.50	0.70	1.00	1.40	1.80
$h_1$	.01547	.03780	.07296	.13673	.19360	.29289	.37996	.50000	.66246	.86327
$h_{12}$	.98453	.96220	.92704	.86327	.80640	.70711	.62004	.50000	.33754	.13673
$h_2$	.03142	.07858	.15740	.31677	.48016	.82843	1.2256	2.0000	3.9252	12.628

$n = 4$										
$w$	0.02	0.05	0.10	0.20	0.30	0.50	0.70	1.00	1.40	1.80
$h_1$	.01188	.02919	.05682	.10812	.15523	.24072	.31928	.43356	.60035	.82855
$h_{12}$	.98812	.97081	.94318	.89188	.84477	.75928	.68072	.56644	.39965	.17145
$h_2$	.02903	.07261	.14544	.29269	.44367	.76547	1.1325	1.8480	3.6269	11.668
$h_{23}$	.98314	.95839	.91859	.84419	.77614	.65585	.55152	.41417	.24835	.08446
$h_3$	.02888	.07168	.14165	.27704	.40762	.66119	.91752	1.3512	2.2538	5.7481
$h_{34}$	.98826	.97163	.94624	.90243	.86563	.80598	.75799	.69757	.62486	.54688
$h_4$	.01174	.02837	.05376	.09757	.13437	.19402	.24201	.30243	.37514	.45312

$n = 5$										
$w$	0.02	0.05	0.10	0.20	0.30	0.50	0.70	1.00	1.40	1.80
$h_1$	.00952	.02316	.04433	.08186	.11442	.16931	.21549	.27639	.35405	.44321
$h_{12}$	.99048	.97684	.95567	.91814	.88558	.83069	.78451	.72361	.64595	.55679
$h_2$	.02527	.06262	.12353	.24107	.35424	.57404	.79624	1.1708	1.9372	4.8059
$h_{23}$	.98444	.96166	.92511	.85682	.79412	.68195	.58247	.44722	.27568	.09597
$h_3$	.03142	.07858	.15740	.31677	.48016	.82843	1.2256	2.0000	3.9252	12.628

TABLE V (Cont'd.)

w	n=6									
	0.02	0.05	0.10	0.20	0.30	0.50	0.70	1.00	1.40	1.80
$h_1$	.00800	.01954	.03767	.07043	.09953	.15005	.19407	.25432	.33508	.43365
$h_{12}$	.99200	.98046	.96233	.92957	.90047	.84995	.80593	.74568	.66492	.56635
$h_2$	.02208	.05474	.10802	.21104	.31056	.50475	.70206	1.0352	1.7101	4.1589
$h_{23}$	.98605	.96560	.93271	.87094	.81371	.70965	.61512	.48241	.30570	.10915
$h_3$	.03035	.07591	.15205	.30600	.46383	.80026	1.1839	1.9320	3.7918	12.198
$h_{34}$	.98386	.96015	.92186	.84966	.78275	.66229	.55585	.41418	.24405	.08125
$h_4$	.03028	.07548	.15028	.29852	.44619	.74686	1.0698	1.6588	3.0271	9.0807
$h_{45}$	.98612	.96600	.93427	.87672	.82575	.73817	.66313	.56152	.42104	.21163
$h_5$	.02195	.05393	.10487	.19904	.28478	.43837	.57767	.77954	1.0829	1.5541
$h_{56}$	.99206	.98083	.96370	.93420	.95948	.86952	.83747	.79724	.74902	.69752
$h_6$	.00794	.01917	.03630	.06580	.09052	.13048	.16253	.20276	.25098	.30248
$h_{n+1-i} = h_i$										
$h_{n-i, n-i+1} = h_{i, i+1}$										
$n=7$										
w	0.02	0.05	0.10	0.20	0.30	0.50	0.70	1.00	1.40	1.80
$h_1$	.00685	.01661	.03169	.05818	.08090	.11869	.14999	.19058	.24125	.29798
$h_{12}$	.99315	.98339	.96831	.94182	.91910	.88131	.85001	.80942	.75875	.70202
$h_2$	.01937	.04765	.09285	.17699	.25438	.39508	.52510	.71758	1.0157	1.5029
$h_{23}$	.98757	.96954	.94099	.88885	.84214	.76055	.68916	.59038	.45046	.23462
$h_3$	.02822	.07025	.13958	.27628	.41170	.68577	.97829	1.5076	2.7229	8.0488
$h_{34}$	.98443	.96157	.92473	.85539	.79115	.67512	.57160	.43146	.25826	.08695
$h_4$	.03142	.07858	.15740	.31677	.48016	.82843	1.2256	2.0000	3.9252	12.628
$n=8$										
w	0.02	0.05	0.10	0.20	0.30	0.50	0.70	1.00	1.40	1.80
$h_1$	.00602	.01466	.02812	.05214	.07313	.10885	.13924	.17977	.23224	.29361
$h_{12}$	.99398	.98534	.97188	.94786	.92687	.89115	.86076	.82023	.76776	.70639
$h_2$	.01727	.04254	.08307	.15905	.22956	.35942	.48135	.66517	.95733	1.4556
$h_{23}$	.98882	.97256	.94672	.89916	.85610	.77972	.71162	.61550	.47636	.25569
$h_3$	.02603	.06477	.12860	.25423	.37847	.62940	.89655	1.3777	2.4711	7.2093
$h_{34}$	.98533	.96378	.92904	.86353	.80261	.69165	.59130	.45262	.27564	.09401
$h_4$	.03082	.07709	.15441	.31075	.47103	.81269	1.2023	1.9620	3.8506	12.388
$h_{45}$	.98411	.96074	.92297	.85159	.78515	.66474	.55753	.41414	.24235	.08012
$h_5$	.03078	.07684	.15340	.30645	.46079	.78107	1.1337	1.7952	3.3855	10.557
$h_{56}$	.98536	.96401	.92995	.86701	.81000	.70966	.62182	.50170	.33927	.13396
$h_6$	.02594	.06420	.12633	.24514	.35809	.57285	.78342	1.1230	1.7600	3.7771
$h_{67}$	.98887	.97287	.94791	.90341	.86473	.79964	.74509	.67322	.57968	.46254
$h_7$	.01718	.04200	.08103	.15159	.21417	.32251	.41667	.54595	.72282	.95311
$h_{78}$	.99402	.98555	.97265	.95045	.93186	.90184	.87778	.84763	.81153	.77303
$h_8$	.00598	.01445	.02735	.04955	.06814	.09816	.12222	.15237	.18847	.22697

TABLE V (Cont'd.)

w	$h_{n+1-i} = h_i$									
	$h_{n-i, n-i+1} = h_{i, i+1}$									
	$n = 9$									
w	0.02	0.05	0.10	0.20	0.30	0.50	0.70	1.00	1.40	1.80
$h_1$	.00534	.01294	.02464	.04509	.06253	.09131	.11496	.14536	.18291	.22441
$h_{12}$	.99466	.98706	.97536	.95491	.93747	.90869	.88504	.85464	.81709	.77559
$h_2$	.01549	.03792	.07336	.13803	.19606	.29812	.38853	.51533	.69390	.93598
$h_{23}$	.98991	.97536	.95255	.91152	.87540	.81360	.76075	.68961	.59453	.47118
$h_3$	.02390	.05913	.11633	.22581	.33008	.52914	.72539	1.0434	1.6401	3.4877
$h_{34}$	.98634	.96641	.93460	.87569	.82208	.72688	.64241	.52494	.36200	.14705
$h_4$	.02946	.07347	.14645	.29172	.43750	.73829	1.0674	1.6811	3.1466	9.7400
$h_{45}$	.98443	.96154	.92461	.85489	.79006	.67242	.56714	.42484	.25113	.08357
$h_5$	.03142	.07858	.15740	.31677	.48016	.82843	1.2256	2.0000	3.9252	12.628
$n = 10$										
w	0.02	0.05	0.10	0.20	0.30	0.50	0.70	1.00	1.40	1.80
$h_1$	.00482	.01172	.02242	.04136	.05776	.08536	.10852	.13897	.17767	.22192
$h_{12}$	.99518	.98828	.97758	.95864	.94224	.91464	.89148	.86103	.82233	.77808
$h_2$	.01408	.03452	.06697	.12664	.18072	.27714	.36400	.48808	.66738	.91954
$h_{23}$	.99079	.97748	.95650	.91845	.88459	.82578	.77460	.70438	.60822	.47947
$h_3$	.02206	.05459	.10744	.20877	.30555	.49116	.67521	.97511	1.5387	3.2518
$h_{34}$	.98728	.96870	.93899	.88378	.83327	.74273	.66136	.54641	.38336	.15995
$h_4$	.02793	.06962	.13864	.27575	.41298	.69522	1.0029	1.5741	2.9291	9.0044
$h_{45}$	.98500	.96295	.92736	.86012	.79748	.68326	.58015	.43883	.26242	.08802
$h_5$	.03103	.07760	.15544	.31281	.47416	.81807	1.2103	1.9750	3.8762	12.470
$h_{56}$	.98423	.96103	.92353	.85256	.78639	.66607	.55852	.41428	.24163	.07963
$h_6$	.03100	.07744	.15479	.31006	.46756	.79749	1.1652	1.8645	3.5691	11.281
$h_{67}$	.98502	.96310	.92796	.86242	.80240	.69543	.60086	.47159	.30189	.10912
$h_7$	.02787	.06921	.13701	.26908	.39768	.65095	.91117	1.3585	2.3066	6.1430
$h_{78}$	.98731	.96893	.93990	.88714	.84024	.75933	.68974	.59542	.46577	.26800
$h_8$	.02198	.05411	.10558	.20165	.29023	.45164	.60124	.82427	1.1784	1.8176
$h_{89}$	.99083	.97770	.95735	.92142	.89051	.83908	.79651	.74123	.67127	.58906
$h_9$	.01401	.03415	.06558	.12172	.17080	.25425	.32522	.42017	.54479	.69615
$h_{910}$	.99520	.98842	.97807	.96028	.94539	.92136	.90211	.87799	.84913	.81839
$h_{10}$	.00480	.01158	.02193	.03972	.05461	.07864	.09789	.12201	.15087	.18161

TABLE VI  
 h VALUES FOR 0.001-DB RIPPLE CHEBYSHEV FILTERS HAVING  $h_0$  AND  $h_{n+1} = 1.0$  AND VARIOUS STOP-BAND 0.001-DB FRACTIONAL BANDWIDTHS  $w$ 

$w$	$h_{n+1-i} = h_i$									
	$h_{n-i, n-i+1} = h_{i, i+1}$									
	$n = 3$									
0.02	0.05	0.10	0.20	0.30	0.50	0.70	1.00	1.40	1.80	
$h_1$	.00638	.01581	.03117	.06081	.08937	.14481	.20033	.29018	.44516	.72075
$h_{12}$	.99362	.98419	.96883	.93919	.91063	.85519	.79967	.70982	.55474	.27925
$h_2$	.01141	.02854	.05718	.11507	.17442	.30093	.44520	.72650	1.4258	4.5869
$h_{n+1-i} = h_i$										
$h_{n-i, n-i+1} = h_{i, i+1}$										
$n = 5$										
0.02	0.05	0.10	0.20	0.30	0.50	0.70	1.00	1.40	1.80	
$h_1$	.00838	.02045	.03935	.07335	.10336	.15507	.19972	.26024	.34027	.43633
$h_{12}$	.99162	.97955	.96065	.92665	.89664	.84493	.80028	.73976	.65973	.56367
$h_2$	.01761	.04399	.08790	.17564	.26378	.44423	.63709	.97773	1.6928	4.2897
$h_{23}$	.99091	.97733	.95481	.91031	.86651	.78056	.69547	.56497	.37232	.13682
$h_3$	.02058	.05148	.10311	.20752	.31455	.54270	.80289	1.3102	2.5714	8.2723
$h_{n+1-i} = h_i$										
$h_{n-i, n-i+1} = h_{i, i+1}$										
$n = 7$										
0.02	0.05	0.10	0.20	0.30	0.50	0.70	1.00	1.40	1.80	
$h_1$	.00901	.02165	.04071	.07292	.09932	.14091	.17334	.21291	.25876	.30593
$h_{12}$	.99099	.97835	.95929	.92708	.90068	.85909	.82666	.78709	.74124	.69407
$h_2$	.01946	.04845	.09610	.18833	.27610	.43939	.59087	.81031	1.1302	1.5942
$h_{23}$	.98972	.97418	.94822	.89704	.84784	.75682	.67444	.56048	.40607	.19396
$h_3$	.02398	.05969	.11869	.23597	.35405	.60021	.87324	1.3866	2.6015	7.9470
$h_{34}$	.98635	.96645	.93468	.87526	.82001	.71775	.62211	.48393	.29840	.10209
$h_4$	.02430	.06078	.12174	.24500	.37138	.64075	.94794	1.5469	3.0360	9.7667
$h_{n+1-i} = h_i$										
$h_{n-i, n-i+1} = h_{i, i+1}$										
$n = 9$										
0.02	0.05	0.10	0.20	0.30	0.50	0.70	1.00	1.40	1.80	
$h_1$	.00923	.02187	.04027	.06968	.09235	.12566	.14981	.17733	.20681	.23476
$h_{12}$	.99077	.97813	.95973	.93032	.90765	.87434	.85019	.82267	.79319	.76524
$h_2$	.02019	.05008	.09844	.18828	.26846	.40372	.51454	.65423	.82239	1.0074
$h_{23}$	.98921	.97279	.94537	.89269	.84481	.76413	.69936	.62054	.53031	.43516
$h_3$	.02510	.06219	.12298	.24290	.36283	.60810	.86733	1.3108	2.1873	5.1708
$h_{34}$	.98574	.96548	.93404	.87694	.82439	.72647	.63417	.50132	.32255	.11839
$h_4$	.02623	.06584	.13247	.26793	.40677	.70042	1.0308	1.6643	3.2129	10.190
$h_{45}$	.98839	.97084	.94141	.88286	.82568	.71667	.61416	.46864	.28138	.09425
$h_5$	.02740	.06854	.13730	.27630	.41882	.72260	1.0690	1.7445	3.4238	11.014

TABLE VII  
 $h$  VALUES FOR 0.001-DB RIPPLE CHEBYSHEV FILTERS HAVING  $h_0$  AND  $h_{n+1}=1.0$  AND VARIOUS STOP-BAND 0.01-DB FRACTIONAL BANDWIDTHS  $w$

$w$	$h_{n+1-i}=h_i$ $h_{n-i,n-i+1}=h_{i,i+1}$ $n=3$									
	0.02	0.05	0.10	0.20	0.30	0.50	0.70	1.00	1.40	1.80
	$h_1$	.00979	.02412	.04718	.09061	.13122	.20672	.27825	.38616	.55251
$h_{12}$	.99021	.97588	.95282	.90939	.86878	.79328	.72175	.61384	.44749	.20113
$h_2$	.01524	.03812	.07636	.15366	.23292	.40187	.59454	.97020	1.9041	6.1256

$w$	$h_{n+1-i}=h_i$ $h_{n-i,n-i+1}=h_{i,i+1}$ $n=5$									
	0.02	0.05	0.10	0.20	0.30	0.50	0.70	1.00	1.40	1.80
	$h_1$	.01161	.02805	.05319	.09664	.13320	.19260	.24052	.30100	.37401
$h_{12}$	.98839	.97195	.94681	.90336	.86680	.80740	.75948	.69900	.62599	.54739
$h_2$	.02056	.05164	.10397	.21045	.31921	.54520	.78913	1.2228	2.1469	5.6562
$h_{23}$	.99132	.97808	.95555	.90934	.86236	.76807	.67433	.53354	.33743	.11888
$h_3$	.02478	.06197	.12414	.24982	.37868	.65334	.96657	1.5773	3.0956	9.9587

$w$	$h_{n+1-i}=h_i$ $h_{n-i,n-i+1}=h_{i,i+1}$ $n=7$									
	0.02	0.05	0.10	0.20	0.30	0.50	0.70	1.00	1.40	1.80
	$h_1$	.01207	.02862	.05279	.09155	.12155	.16585	.19811	.23503	.27477
$h_{12}$	.98793	.97138	.94721	.90845	.87845	.83415	.80189	.76497	.72523	.68738
$h_2$	.02200	.05533	.11126	.22183	.32791	.52278	.69744	.93756	1.2609	1.6795
$h_{23}$	.99037	.97503	.94776	.89024	.83269	.72539	.63067	.50593	.34905	.15468
$h_3$	.02723	.06733	.13267	.26030	.38734	.65143	.94608	1.5067	2.8562	8.8674
$h_{34}$	.98228	.95702	.91790	.84816	.78635	.67715	.57907	.44224	.26659	.08970
$h_4$	.02565	.06416	.12853	.25866	.39207	.67645	1.0008	1.6331	3.2051	10.311

$w$	$h_{n+1-i}=h_i$ $h_{n-i,n-i+1}=h_{i,i+1}$ $n=9$									
	0.02	0.05	0.10	0.20	0.30	0.50	0.70	1.00	1.40	1.80
	$h_1$	.01217	.02837	.05102	.08509	.10971	.14359	.16656	.19128	.21619
$h_{12}$	.98783	.97163	.94898	.91491	.89029	.85641	.83344	.80872	.78381	.76159
$h_2$	.02259	.05684	.11360	.22064	.31526	.46864	.58677	.72572	.87959	1.0341
$h_{23}$	.98988	.97323	.94321	.88189	.82530	.73280	.66300	.58408	.50127	.42157
$h_3$	.02787	.06829	.13343	.26147	.39197	.66934	.97416	1.5102	2.5978	6.4690
$h_{34}$	.98214	.95809	.92335	.86551	.81485	.71965	.62644	.48889	.30576	.10825
$h_4$	.02717	.06883	.14022	.28834	.44210	.76889	1.1369	1.8437	3.5788	11.409
$h_{45}$	.99148	.97761	.95229	.89691	.83922	.72540	.61750	.46611	.27621	.09175
$h_5$	.02994	.07488	.14998	.30183	.45752	.78937	1.1678	1.9057	3.7401	12.032

TABLE VIII  
 $h$  VALUES FOR 0.1 DB RIPPLE CHEBYSHEV FILTERS HAVING  $h_0$  AND  $h_{n+1} = 1.0$  AND VARIOUS STOP-BAND 0.1-DB FRACTIONAL BANDWIDTHS  $w$

$h_{n+1-i} = h_i$ $h_{n-i, n-i+1} = h_{i, i+1}$ $n = 3$										
$w$	0.02	0.05	0.10	0.20	0.30	0.50	0.70	1.00	1.40	1.80
$h_1$	.01595	.03895	.07509	.14043	.19849	.29936	.38729	.50775	.66936	.86689
$h_{12}$	.98405	.96105	.92491	.85957	.80151	.70064	.61271	.49225	.33064	.13311
$h_2$	.01802	.04508	.09030	.18173	.27547	.47527	.70313	1.1474	2.2519	7.2444

$h_{n+1-i} = h_i$ $h_{n-i, n-i+1} = h_{i, i+1}$ $n = 5$										
$w$	0.02	0.05	0.10	0.20	0.30	0.50	0.70	1.00	1.40	1.80
$h_1$	.01739	.04133	.07645	.13323	.17755	.24360	.29214	.34819	.40911	.46770
$h_{12}$	.98261	.95867	.92355	.86677	.82245	.75640	.70786	.65181	.59089	.53230
$h_2$	.02184	.05570	.11477	.24131	.37710	.67240	1.0023	1.6024	2.9173	8.1267
$h_{23}$	.99617	.98936	.97548	.94033	.89822	.80262	.70050	.54436	.33347	.11391
$h_3$	.03103	.07760	.15544	.31281	.47416	.81807	1.2103	1.9750	3.8762	12.470

$h_{n+1-i} = h_i$ $h_{n-i, n-i+1} = h_{i, i+1}$ $n = 7$										
$w$	0.02	0.05	0.10	0.20	0.30	0.50	0.70	1.00	1.40	1.80
$h_1$	.01758	.04073	.07269	.11982	.15322	.19825	.22823	.25997	.29143	.31907
$h_{12}$	.98242	.95927	.92731	.88018	.84678	.80175	.77177	.74003	.70857	.68993
$h_2$	.02298	.05948	.12424	.26024	.39467	.63830	.84496	1.1064	1.4196	1.7691
$h_{23}$	.99524	.98487	.96081	.89735	.82625	.69022	.57492	.43511	.27905	.11263
$h_3$	.03215	.07781	.14880	.27950	.40417	.65899	.94530	1.5008	2.8685	9.0265
$h_{34}$	.97199	.93375	.87813	.78827	.71650	.60184	.50671	.38050	.22532	.07492
$h_4$	.02472	.06182	.12382	.24919	.37772	.65168	.96412	1.5733	3.0878	9.9334

$h_{n+1-i} = h_i$ $h_{n-i, n-i+1} = h_{i, i+1}$ $n = 9$										
$w$	0.02	0.05	0.10	0.20	0.30	0.50	0.70	1.00	1.40	1.80
$h_1$	.01747	.03954	.06836	.10775	.13362	.16613	.18640	.20677	.22593	.24199
$h_{12}$	.98253	.96046	.93164	.89225	.86638	.83387	.81360	.79323	.77407	.75801
$h_2$	.02359	.06174	.12920	.26248	.37938	.55700	.68092	.81264	.94328	1.0612
$h_{23}$	.99451	.98120	.94999	.87487	.80297	.69180	.61627	.53992	.46890	.40778
$h_3$	.03198	.07557	.14179	.26884	.40394	.71890	1.0976	1.8044	3.3008	8.8634
$h_{34}$	.97290	.94013	.89990	.84795	.81051	.73782	.65347	.51178	.31400	.10796
$h_4$	.02622	.06837	.14470	.31307	.49447	.88463	1.3225	2.1595	4.2141	13.488
$h_{45}$	1.0031	1.0038	.99651	.96023	.90822	.78921	.66997	.50190	.29457	.09727
$h_5$	.03464	.08665	.17356	.34929	.52945	.91347	1.3514	2.2053	4.3281	13.924

TABLE IX

h VALUES FOR 0.5-DB RIPPLE CHEBYSHEV FILTERS HAVING  $h_0$  AND  $h_{n+1}=1.0$  AND VARIOUS STOP-BAND 0.5-DB FRACTIONAL BANDWIDTHS

w	$h_{n+1-i} = h_i$									
	$h_{n-i, n-i+1} = h_{i, i+1}$									
$n=3$										
$h_1$	.02446	.05902	.11161	.20181	.27706	.39803	.49449	.61484	.75804	.90974
$h_{12}$	.97554	.94098	.88839	.79819	.72294	.60197	.50551	.38516	.24196	.09026
$h_2$	.01723	.04309	.08631	.17370	.26329	.45427	.67206	1.0967	2.1524	6.9243

$$h_{n+1-i} = h_i$$

$$h_{n-i, n-i+1} = h_{i, i+1}$$

$$n=5$$

w	$h_{n+1-i} = h_i$									
	$h_{n-i, n-i+1} = h_{i, i+1}$									
$n=5$										
$h_1$	.02543	.05910	.10583	.17540	.22513	.29280	.33822	.38666	.43503	.47782
$h_{12}$	.97457	.94090	.89417	.82460	.77487	.70720	.66178	.61334	.56497	.52218
$h_2$	.01997	.05231	.11219	.25189	.41416	.79356	1.2404	2.0805	3.9695	11.643
$h_{23}$	1.0068	1.0147	1.0221	1.0183	.99536	.91300	.80488	.62532	.37833	.12742
$h_3$	.03991	.09983	.19997	.40242	.60999	1.0524	1.5570	2.5408	4.9866	16.042

$$h_{n+1-i} = h_i$$

$$h_{n-i, n-i+1} = h_{i, i+1}$$

$$n=7$$

w	$h_{n+1-i} = h_i$									
	$h_{n-i, n-i+1} = h_{i, i+1}$									
$n=7$										
$h_1$	.02522	.05665	.09695	.15073	.18526	.22781	.25385	.27967	.30365	.32350
$h_{12}$	.97478	.94335	.90305	.84927	.81474	.77219	.74615	.72033	.69635	.67650
$h_2$	.02110	.05738	.12787	.29063	.45917	.75958	.99691	1.2688	1.5559	1.8356
$h_{23}$	1.0055	1.0065	.99241	.92515	.83515	.65888	.51872	.36589	.21727	.08087
$h_3$	.03926	.09135	.16530	.28646	.39263	.60264	.84106	1.3163	2.5161	7.9686
$h_{34}$	.95394	.89420	.81345	.69706	.61514	.50011	.41440	.30731	.18023	.05959
$h_4$	.02112	.05282	.10581	.21293	.32276	.55687	.82385	1.3444	2.6385	8.4882

$$h_{n+1-i} = h_i$$

$$h_{n-i, n-i+1} = h_{i, i+1}$$

$$n=9$$

w	$h_{n+1-i} = h_i$									
	$h_{n-i, n-i+1} = h_{i, i+1}$									
$n=9$										
$h_1$	.02477	.05394	.08882	.13146	.15675	.18590	.20275	.21876	.23304	.24447
$h_{12}$	.97523	.94606	.91118	.86854	.84325	.81410	.79725	.78124	.76696	.75553
$h_2$	.02194	.06137	.13866	.30266	.44530	.64487	.76870	.88706	.99296	1.0804
$h_{23}$	1.0041	.99909	.96934	.87568	.78303	.65106	.57233	.50185	.44351	.39791
$h_3$	.03777	.08345	.14515	.25794	.38684	.73311	1.2051	2.1578	4.2675	12.327
$h_{34}$	.95679	.91017	.86294	.82462	.81376	.79130	.73297	.59119	.36317	.12321
$h_4$	.02311	.06351	.14413	.34184	.56918	1.0698	1.6282	2.6823	5.2546	16.852
$h_{45}$	1.0257	1.0560	1.0875	1.0970	1.0626	.93991	.80021	.59803	.34942	.11505
$h_5$	.04279	.10702	.21438	.43142	.65395	1.1283	1.6692	2.7239	5.3460	17.198